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Structural Stability of the High-Aluminium Zinc Alloys Modified with Ti Addition

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Abstract

The subject of the paper is structural stability of the Zn-26 wt.% Al binary alloys doped with 2.2 wt.% Cu or 1.6 wt.% Ti addition. The structural stability of Zn-Al alloys with increased Al content is connected with stability of solid solution of zinc in aluminium a', which is the main component of these alloys microstructure. Such a solution undergoes phase transformations which are accompanied, among others, by changes in dimensions and strength properties.

The structural stability of the ZnAL26Cu2.2 and ZnAl26Ti1.6 alloys was investigated using XRD examinations during long term natural ageing after casting, as well as during long term natural ageing after super-saturation and quenching. On the basis of the performed examinations it was stated that small Ti addition to the binary ZnAl25 alloy, apart from structure refinement, accelerates decomposition of the primary α' phase giving stable structure in a shorter period of time in comparison with the alloy without Ti addition. Addition of Ti in amount of 1.6 wt.%, totally replacing Cu, allows obtaining stable structure and dimensions and allows avoiding structural instability caused by the metastable ε–CuZn₄ phase present in the ZnAl26Cu2.2 alloy.

Keywords: High Aluminium Zinc alloys, Ti addition, Structural stability, XRD examinations

1. Introduction

Zinc based cast alloys have good mechanical and technological properties, therefore they are commonly used in industry. These alloys can be gravity cast into sand, semipermanent and metal moulds, and their main application is in production of machines and parts of devices. Technology of casting of zinc alloys covers continuous, semi-continuous, centrifugal and investment casting as well as casting under pressure. In recent years, zinc-based alloys have been also used for semi-solid casting, e.g. squeeze casting [1-2]. Alloys based on Zn-Al with the increased amount of Al are generally stronger than most of the Al alloys, they have bearing properties and wear

resistance similar to those of bearing bronzes, they have better tooling properties and display mechanical properties similar to those of numerous types of cast iron. Investigations on Zn-Al alloys of increased content of Al result from several disadvantageous characteristics of these alloys, i.e. relatively low value of allowable operating temperature, susceptibility to gas porosity, great sensitivity to overheating of liquid metal leading to oxidation of alloy components, instability of structure and dimensions caused by phase transformations which take place in solid alloys over long periods of time after casting, as well as susceptibility to developing coarse grain structure of the sandcastings; the latter causes difficult feeding and decrease of elongation [3].

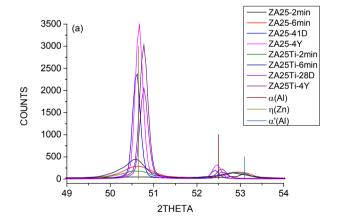
The phase transformations are connected with solid solution of zinc in aluminium α , which is the main component of these alloys microstructure. Such a solution undergoes phase-transformations which are accompanied by, among others, changes in dimensions, electrical resistance and strength properties.

Numerous papers on investigations of structural stability, phase transformations and their effect on the Zn-Al alloys properties include, among others, influence of Cu [4-5], RE [6-8] and Ti [9-12].

In paper [4] it was found that addition of Cu prolongs process of decomposition in the alloy Al-78wt%Zn-(1-3) wt.% Cu in room temperature to about half a year. It should be pointed out that the metastable ϵ -CuZn₄ phase takes part in the so-called fourphase reaction to form a stable T'-Al₅Cu₄Zn phase. However, the four-phase reaction can lead to an increase of volume of the Zn-Al-Cu alloys even by 4.5 % [5].

In the papers [6-7] the effect of rare earth elements (RE) on the course of ageing of the alloy ZA-27 was investigated. It was determined that the addition of up to 0.3 wt% of RE (mainly La, Ce and Nd) does not influence the sequence of phase transformations observed in supersaturated alloy ZA27 without RE addition [8].

The effect of a small (0.04 wt%) Ti addition on the structural stability of high-aluminium zinc alloys was investigated in the papers [9-12]. The investigations were carried on the alloy Zn-25wt%Al, which is the base of the ZA27 alloy and its Polish analogue Z284.



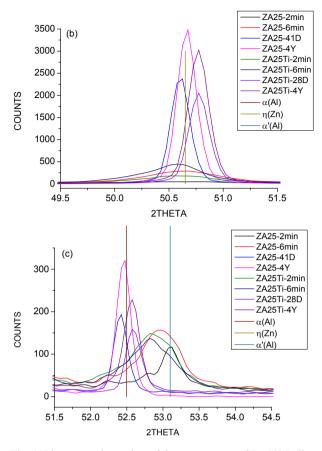


Fig. 1. Phase transformation of the supersaturated ZnAl25 alloy without Ti addition (ZA25) and with 0.04 wt% Ti addition (ZA25Ti); min, D, Y denotes time after quenching in, accordingly, minutes, days and years

During these examinations samples of the Zn-25wt%Al after supersaturation at 370°C/48 hours were quenched in water of room temperature, and then directly used in the XRD examinations. It was determined that the alloy Zn-25wt%Al with the addition of Ti undergoes phase changes in a shorter time after quenching than in the case of the same alloy without the addition of Ti [9], [11] - Fig. 1. This can suggest that Ti intensifies initial stage of the phase transformations, i.e. decomposition of the primary a' solid solution. On the other hand, the examined ZnAl25 with Ti addition did not display dimensional changes during natural ageing after supersaturation and quenching [10], [12]. This suggests that Ti addition stabilizes the α phase. As it was mentioned above, the Cu addition, which beneficially influences strength and wear properties of the Zn-Al alloys, forms metastable ε-CuZn₄ phase. The ε-CuZn₄ phase transforms to stable T' Al₅Cu₄Zn phase through the mentioned four-phase reaction, which causes significant dimension changes. That is why the Zn-Al-Cu alloys should be thermally treated before introducing them into application, which increases final cost of the castings.

The present initial work is devoted to examining the possibility of obtaining structural stability of the ZnAl26 alloy through total replacing Cu with Ti addition.

2. Experimental procedure

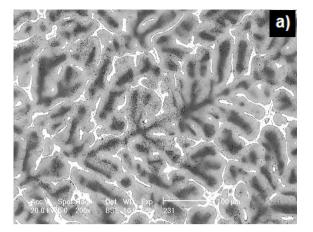
Examined alloys Zn-26wt%Al-2.2wt%Cu (ZnAl26Cu2.2), Zn-26wt%Al-1.6wt%Ti (ZnAl26Ti1.6) and master alloys Al-12.5wt%Ti (AlTi12) and Al-33wt%Cu (AlCu33) were melted from electrolytic aluminium (minimum purity 99.96%), electrolytic zinc (99.995%), electrolytic copper (99.95%) and titanium sponge (98-99.8%, from Johnson Matthey Alfa). The Zn-Al alloys were melted in an electric resistance furnace, in an alumina crucible of 0.2 liter capacity. The AlTi12 and AlCu33 master alloys were melted in a Balzers induction furnace with a protective argon atmosphere. The melts of ZnAl26 alloys were superheated to about 600 °C and the AlTi12 0r AlCu33 master alloys were added to give an overall Ti content of 1.6 wt.% (ZnAl26Ti1.6) and 2.2 wt.% Cu (ZnAl26Cu2.2). Five minutes after one master alloys addition, the bath was stirred for 2 minutes with an alumina rod, and the alloys were cast into a dried sand mould with vertical cylindrical cavity Ø30 x 80 mm. From the middle part of castings samples about 25 mm high were cut for structural and XRD examinations. After grinding (on SiC grades 200, 400, 600, 800 and 1000) they were polished using 6 µm and 1 μm diamond paste and finally using a suspension of 0.5 μm alumina in water-ethanol. Scanning electron microscopy (SEM) investigations were performed on unetched samples using Philips XL30 microscope equipped with an energy dispersive X-ray EDX spectrometer Link-Isis. X-ray diffraction investigations were made at 2Θ range of 20-130° with diffractometer Philips PW1710 and Co Kα radiation filtered by graphite at {002} plane. Step measurement was carried at parameters step/time = 0.02°/10 s. Analysis of the obtained X-ray patterns was made with the use of computer software Philips PC-APD.

3. Results

3.1. Zn-Al and Zn-Al-Cu alloys

The initial microstructure of the binary ZnAl26 alloy poured into a sand mould is shown in Fig. 2(a). Fig 2(b) shows the microstructure obtained in the same conditions, but after addition of the 0.04 wt.% Ti, introduced into the melt with the Zn-4wt%Ti master alloy (ZnTi4 MA). Furthermore, Fig. 2(b) clearly shows significant refinement of the dendritic structure of the α (Al) solid solution, which should positively influence plastic properties of the inoculated alloy. On basis of the previous publications [13-15] the observed refinement appears due to heterogeneous nucleation of the α ' solid solution on the (Al,Zn)₃Ti nucleants, originated from the Zn₃Ti present in the ZnTi4 MA.

Similar picture of dendritic structure of the ZnAl26Cu2.2 alloy is shown in Fig. 3(a). It is slightly refined and more compacted in comparison with the binary ZnAl26 one shown in Fig. 2 (a).



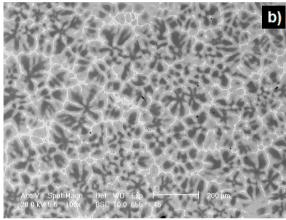


Fig. 2. SEM picture of the ZnAl25 sand cast alloy, (a) – initial alloy, non-inoculated; visible coarse dendritic structure; (b) the same ZnAl25 alloy inoculated with 400 ppm Ti, introduced to the melt with a ZnTi4 MA

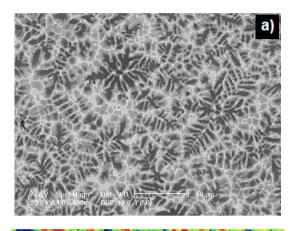
The maps of elements distribution presented in Fig. 3(b)-(d) show, that Cu remains with Zn mainly in the α (Al) solid solution. Furthermore, in the ZnAl26Cu2.2 alloy examined a few days after pouring the samples there are no visible particles of the binary ϵ -cuzn4 phase and no peaks coming from this phase are present in the XRD patterns, shown in Fig. 4.

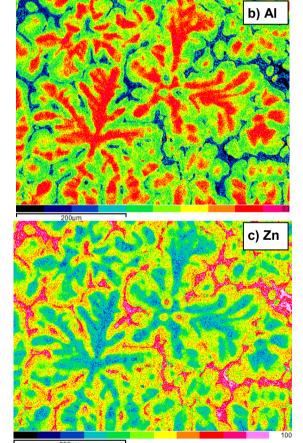
On the other hand, the same alloy examined after 1.5 year of natural ageing has the metastable ϵ - $_{CuZn4}$ phase in its structure, which was stated during the XRD examinations – Fig. 4.

3.2. Zn-Al-Ti alloys

The structure of the examined ZnAl26 alloy after total replacing Cu with Ti addition is shown in Fig. 5. In the ZnAl26Ti1.6 microstructure there are visible cored dendrites of the $\alpha(Al)$ phase, $\eta(Zn)$ phase and also Ti(Al,Zn)₃ particles, evolved in-situ from the Al₃Ti ones. The Al₃Ti particles were introduced into the ZnAl26 melt with the AlTi12 MA. It should be noted, that the Ti(Al,Zn)₃ particles should play the same bearing role as the metastable ϵ -CuZn4 and stable T' Al₅Cu₄Zn phases in the ternary Zn-Al-Cu alloys do. However, contrary to

the ZnAl26Cu2.2 alloy, the ZnAl26Ti1.6 alloy does not show any new phases, even after 1.5 year of the natural ageing – which is clearly visible in the XRD traces presented in Fig. 6. This can suggest that replacing Cu with Ti can be beneficial for obtaining stable structure and dimensions of the high-aluminium zinc alloys.





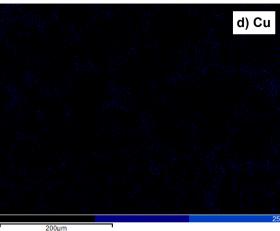
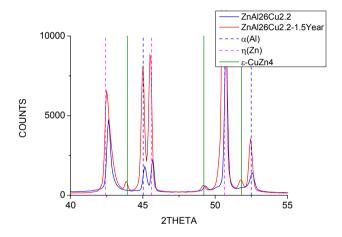


Fig. 3. SEM BSE picture of the ZnAl26Cu2.2 alloy (a) and surface distribution of Al (b), Zn (c) and Cu (d)



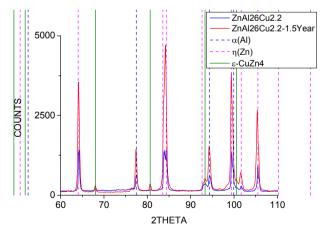
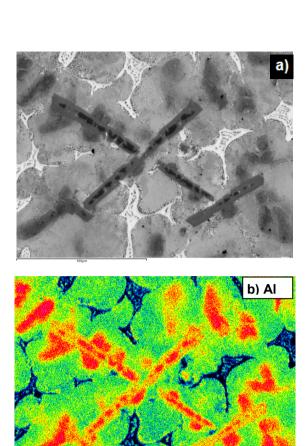
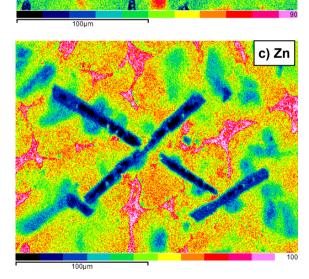


Fig. 4. XRD traces of the ZnAl26Cu2.2 alloy. Invisible ϵ –CuZn₄ peaks for the alloy examined in a few days after pouring. Visible ϵ –CuZn₄ peaks arising during long term (1.5 year) natural ageing – ZnAl26Cu2.2–1.5Year





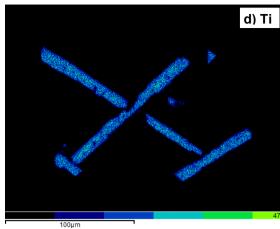
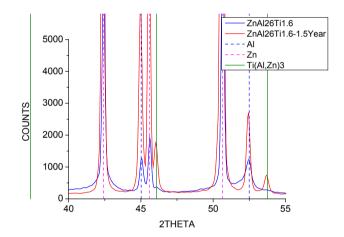


Fig. 5. SEM BSE picture of the ZnAl26Ti1.6 alloy (a) and surface distribution of Al (b), Zn (c) and Ti (d)



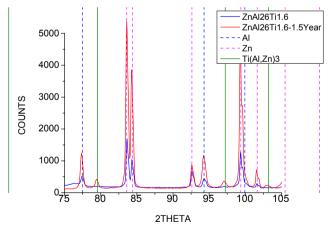


Fig. 6. XRD traces of the ZnAl26Ti1.6 alloy made directly after sample pouring and made after 1.5 year of the natural ageing



4. Conclusions

On basis of the presented results the following conclusions can be formulated:

- Replacement of Cu with Ti, introduced with the AlTi12
 master alloy, evolves in situ Ti(Al,Zn)₃ particles in
 microstructure of the examined ZnAl26Ti1.6 alloy. These
 particles should act as the reinforcing and the bearing ones of
 the ZnAl26-type alloys, designed for tribological applications.
- The ZnAl26Ti1.6 alloy appears to have stable structure (and dimensions) which was stated on the basis of the XRD examinations performed in long-term period of 1.5 year after samples casting. This is a positive achievement of this replacement.
- The influence of the total Cu with Ti replacement on strength and tribological properties should be the subject of detailed examinations.
- 4. The influence of partial replacement of Cu with Ti on structural stability and properties of the high-Al zinc alloys should be also a subject of investigations. This will be discussed elsewhere [18].

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