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A NON-DESTRUCTIVE EVALUATION OF MICROSTRUCTURAL ANALYSIS IN Sn-Ag-Cu SOLDER JOINT BY SYNCHROTRON X-RAY RADIATION TOMOGRAPHY

This paper demonstrates a non-destructive technique to evaluate the internal microstructure in the Sn-Ag-Cu (SAC) solder joint through synchrotron X-ray radiation tomography. Synchrotron X-ray tomography is increasingly utilized for characterizing the internal microstructure of materials in 3D images. A 3D model is reconstructed from a set of 2D projection images taken from different angles and angular position during the sample rotation, thus it could provide a more comprehensive description of the microstructure of an alloy compared to 2D images. In this paper, it is successfully observed and evaluated the internal microstructure of a 900 μm solder joint sample. The key principles and methods of synchrotron X-ray tomography are briefly described. Examples of quantitative and qualitative assessments on the grain refinement effect of Mg addition to SAC35 solder joint are also presented in this paper.

Keywords: Synchrotron tomography; SPring-8; Solder joint; 3D microstructure

1. Introduction

The development, application, and widespread use of tomography of materials and structures has been tremendous growth in the material science industry [1-5]. Synchrotron X-ray radiation has high brightness, high flux, and high collimation characteristic, allowing it to generate higher brilliance than that of lab-based X-ray [6]. The lab-based X-ray is typically produced by bombarding the anode with fast-moving electrons, resulting in 30-150 kV X-rays energy. On other hand, synchrotron X-ray is generated by dedicated synchrotron particles. The charged electrons in the synchrotron are accelerated to extremely high speed in the booster ring, then are transferred to closed loop storage ring by strong magnets. Along the circulating path, specific bending magnets or insertion devices are inserted to cause the radial acceleration of the electrons, producing synchrotron radiation tangential to the ring. With the advanced technique, synchrotron X-ray can be produced up to 8 GeV energies at Super Photo Ring (SPring-8), Japan.

Synchrotron X-ray radiation tomography technique has been increasingly applied in the studies of materials science and engineering. It is a technique that can non-destructively detect

and characterize the internal microstructure of the alloy [7]. The principle of synchrotron tomography is based on the generation of 2D X-ray images by directing an X-ray beam from synchrotron light source and passes through the sample [8]. Further, a charge-coupled device (CCD) detector receives a large number of radiographic images at various angular positions during 360° rotation of the sample. After that, these 2D X-ray images are then reconstructed using reconstruction algorithms and software. The filtered back-projection algorithm is a commonly used procedure for image reconstruction [9]. The field of view is initially cropped to reduce the file size for reconstructions.

There is a fast and exciting growth of research outputs and progress by tomography scientists, researchers and industries. This technique provides an insight into the internal microstructure of materials in 3D model without destructing the sample, with minimal sample preparation. Compared to the 2D images obtained by optical and scanning electron microscopy, which have been shown to misrepresent the statistics of 3D microstructure [10]. 3D visualization provides more reliable qualitative and quantitative outputs. For instance, spatial distribution, particle volume, morphology of the particles, defect distribution in a sample could be rendered and measured. These provide

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fundamental insight into microstructure, correlating to the mechanical performance.

It has been reported that the reliability of the solder joint is depending on the microstructure [11]. Hence, it is crucial to understand the internal microstructure of a solder joint for predicting the life span and reliability during its application. Many studies have conducted finite element (FE) models to predict the mechanical behavior of the solder joints [10]. However, there is still a certain gap between actual situation and stimulated situation, as many settings such as the size and distribution in the solder joints are randomly set [12]. Therefore, the synchrotron tomography plays a crucial role as it could provide more detailed information. Due to the fact of high brilliance and high coherency of monochromatized X-ray at Spring-8, it is possible to obtain high resolution, high spatial resolution, and high contrast in its projection images. Salleh et al. have reported that 29 keV X-rays energy generated by synchrotron radiation is sufficient to detect the contrast between Sn, Cu, and Cu_6Sn_5 due to their dissimilar densities [13].

High Cu-content in solder alloys suitable for high temperature application, such as in engine components and braking system [14-16]. However, the addition of Cu content in Sn-based solder alloy may lead to the formation of large and massive Cu_6Sn_5 . Cu_6Sn_5 was reported that will undergo polymorphic transformation from monoclinic to hexagonal at temperature around 186°C, which may threaten the mechanical and reliability of solder joints [17-20]. Previous studies have shown that the addition of alloying element/reinforced with nano powder can refine and stabilize the Cu_6Sn_5 phase [21-24]. Therefore, this paper is aimed to demonstrate the ability of synchrotron techniques to be used to observe the grain refinement effect of Sn-3wt%Ag-5wt%Cu due to minor addition of Mg in BGA scale solder joint.

2. Methodology

Materials and sample preparation. The solder alloys used in this research are Sn-3wt%Ag-5wt%Cu (SAC35) and Sn-3wt%Ag-5wt%Cu-0.10wt%Mg (SAC35-0.10wt%Mg). The procedure for preparing the solder alloys was described elsewhere [14]. To prepare the BGA-scaled solder joint, the

solder sheet was rolled into 0.054 mm and punched into a disc shaped with 3 mm diameter. The disc-shaped solder sheets were heated to form 900 μm solder balls, sieving is needed to ensure the homogeneity of the size of solder balls. Then, the solder ball was placed on the printed circuit board (PCB) Cu substrate with a little smear of rosin mildly activated (RMA) flux. The PCB was then reflowed under the reflow temperature: the maximum temperature 250°C for 60s and cooled at a rate of 0.33°C/s. The residual of the flux was subsequently cleaned using acetone.

Experiment setup, process, and image reconstruction.

The synchrotron X-rays tomography was conducted at beam-line BL20XU at the SPring-8 synchrotron radiation facility, Japan. During the experiment, a 900 μm solder joint was glued on a zirconia tube, as per Fig. 1(a). The experimental setup for the tomography test is shown in Fig. 1(b). Monochromatized X-rays with energy, 29 keV were used on a sample rotated at 4s/rotation. Beam energy selection for Sn-based alloy was described elsewhere [13]. The incident beam was adjusted to 5 mm in width and 3mm in height to obtain the transmission images. The transmission images were captured by beam monitor with a pixel size of 6.5 $\mu\text{m} \times 6.5 \mu\text{m}$ at a rate of 3 fps. The distance of the beam monitor was 0.5 m away from the solder joint sample. Reconstruction of transmission images was done using 250 projected images over 180° by convolution back-projection method. The selected reconstruction area was the near center of the solder joint specimen. The reconstructed images were further rendered using ImageJ software to noise filtering as well as normalization as to enhance the quality of the images. Using the reconstructed images, a quantitative analysis of the internal microstructure in the SAC35 and SAC3-0.10wt%Mg solder joints was performed.

3. Result and discussions

By using SEM, it was found that minor addition (0.10wt%) of Mg into SAC35 solder alloys significantly refined the primary Cu_6Sn_5 particles. Fig. 2(a) and (b) show the SEM micrographs of SAC35 and SAC35-0.10wt%Mg solder alloy under as-casted conditions respectively. The black particles as shown in Fig. 2 are the primary Cu_6Sn_5 particles. It can be seen that there are some long rod-like particles present in SAC35 solder alloy, whereas, in SAC35-0.10wt%Mg solder alloy, the primary Cu_6Sn_5 particles

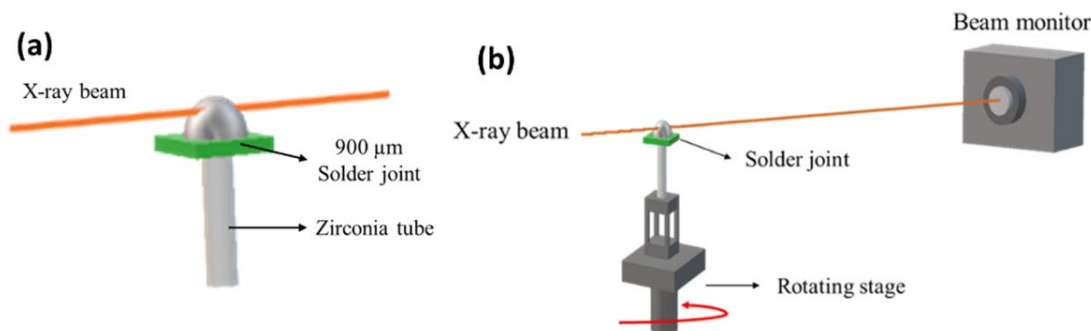


Fig. 1. (a) Sample set up: The alloy was soldered on a PCB substrate and placed on top of a zirconia tube then fixed on the rotating stage. (b) Schematics illustration of synchrotron X-rays tomography at BL20XU, SPring-8, Japan

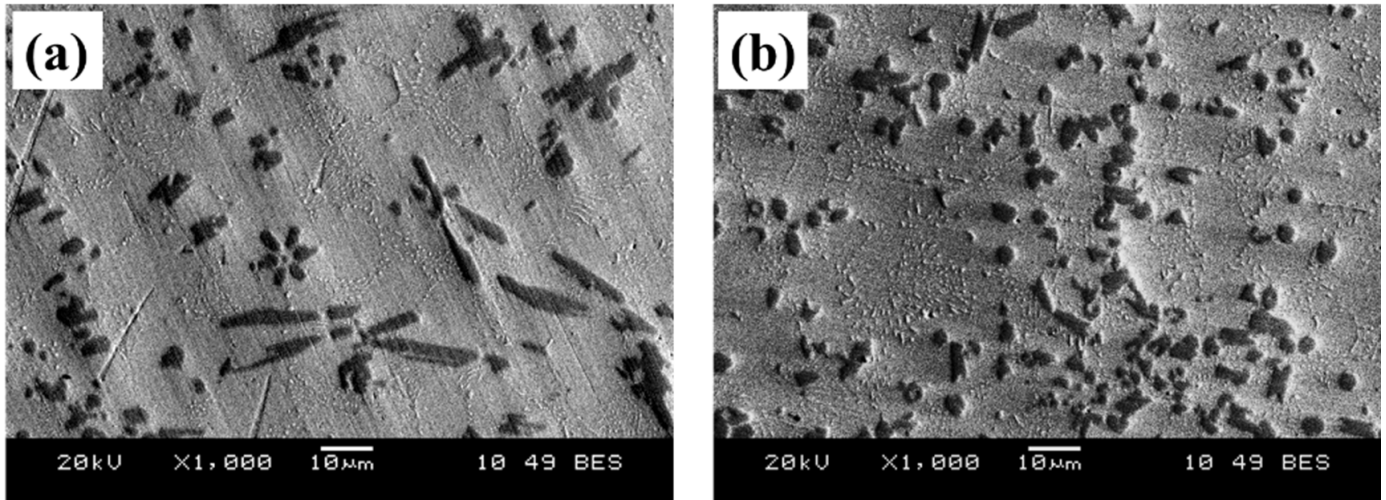


Fig. 2. SEM micrographs of (a) SAC35 and (b) SAC35-0.10wt%Mg solder alloys

are refined and shorter. A preliminary conclusion based on the 2D SEM micrographs is that the minor addition of MG could help to refine the primary Cu_6Sn_5 particles in SAC35 solder alloy. An in-depth study on the microstructural analysis was then conducted using synchrotron tomography technique.

Owing to high X-rays energy at BL20XU in SPring-8, it is sufficient contrast and resolution to observe the primary intermetallic compounds (IMCs) in the BGA-scaled SAC35-xMg solder joint. Fig. 3(a) shows the 3D reconstructed images at the near center of SAC35, and Fig. 3(b) represents SAC35-0.10wt%Mg solder joints under as-reflowed conditions. The green particles represent the primary IMCs that formed in the solder joints. The quantitative measurements were executed to calculate the number and mean volume of Cu_6Sn_5 particles in the selected area. There was approximately a total of 660 Cu_6Sn_5 particles were found in SAC35 sample (Fig. 2a), whereas it reduces to about 170 Cu_6Sn_5 particles with 0.10wt% Mg added to SAC35 (Fig. 2b). However, the minimum volume that can be traced by this technique is set

to $10\ \mu\text{m}^3$. Therefore, it is believed that some diminutive Cu_6Sn_5 particles are untraceable in SAC35-0.10wt%Mg solder alloy. Besides, the mean volume of Cu_6Sn_5 particles was also reduced by 25% with only 0.10wt% Mg addition.

In addition, it is also sufficient resolution to render and focus on a single IMC. This allows the observation of more details on the morphology and shape of the IMCs formed. Fig. 4(a-e) reveals the morphology of primary IMCs that was found in the solder joint of SAC35 and SAC35-0.10wt% Mg. The primary IMC, typically formed in SAC solder alloy, is identified as Cu_6Sn_5 and usually appears in a coarse and long-rod shaped morphology, which is nonoptimal for the reliability performance of a solder joint. It was found that the morphology of the primary Cu_6Sn_5 particles was become shorter and rounder after the presence of 0.10wt% of Mg addition, as per Fig. 4(d&e). Therefore, a clearer observation of the morphology of the primary IMCs allows the researchers to have better predictions of the mechanical properties and the failure mechanism is possible to be predicted.

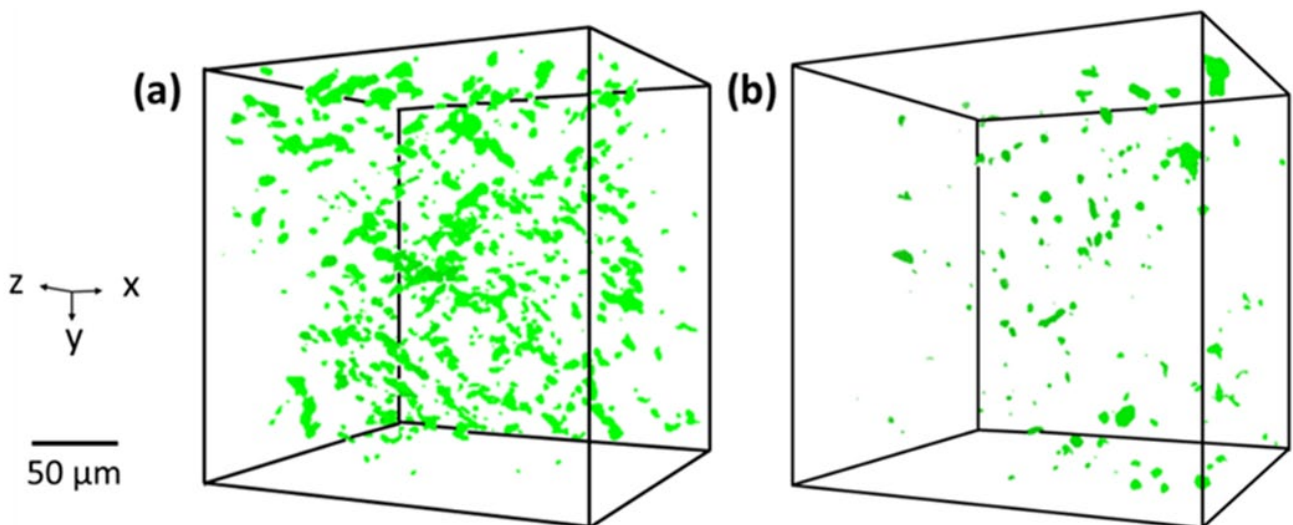


Fig. 3. Comparison of internal IMCs in the solder joint of (a) SAC35 and (b) SAC35-0.10Mg. Green particles are representing the primary Cu_6Sn_5 particles that formed in the solder joints

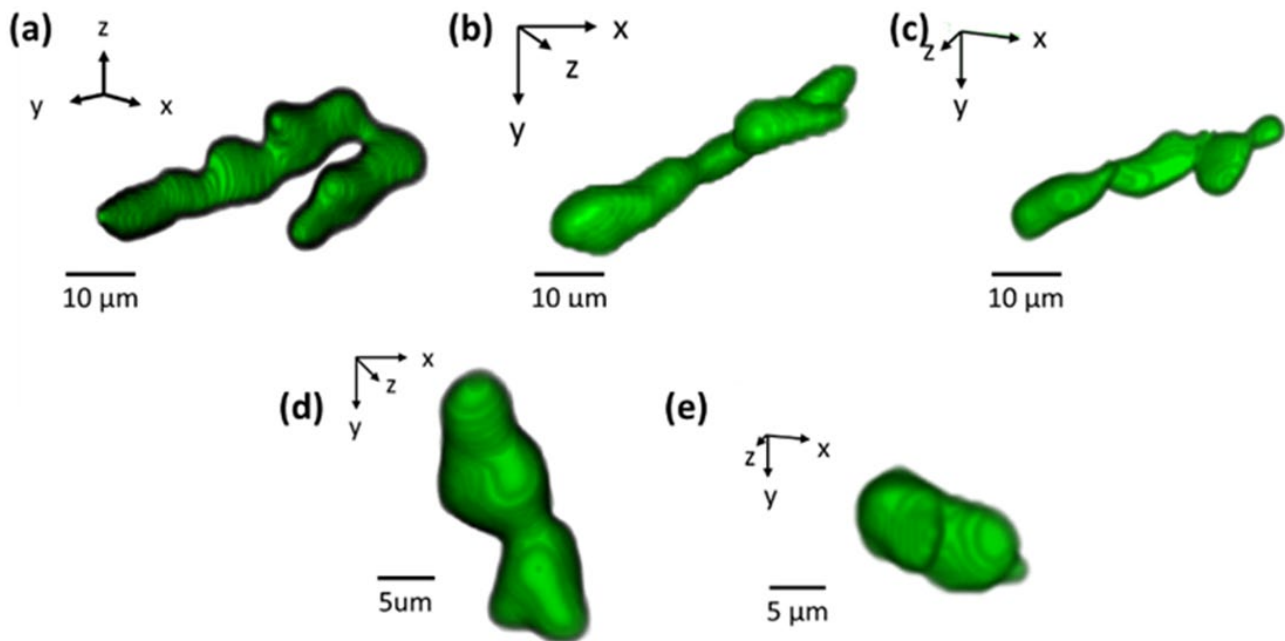


Fig. 4. 3D rendering on primary Cu_6Sn_5 found in (a-c) C and (d&e) SAC35-0.10wt%Mg solder joint

4. Conclusion

This experiment was successful and had sufficient contrast to differentiate primary Cu_6Sn_5 and matrix $\beta\text{-Sn}$ phases. The experiment results show the ability of Mg to refine SAC35 alloy in 900 μm solder joint. This paper highlighted the potential of the use of the synchrotron X-ray tomography technique on the microstructural analysis on BGA scaled solder joint samples. This experiment was performed to evaluate the feasibility of using high energy (29 keV) synchrotron X-rays tomography technique to observe and measure the internal microstructure of primary Cu_6Sn_5 in the SAC35 solder alloys. Based on the results obtained, it is sufficient to observe the grain refinement on SAC35 solder alloy due to the addition of 0.10 wt% Mg.

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