#### ARCHIVES OF METALLURGY

Volume 45 2000 Issue 2

## STANISŁAW MAŁECKI\*, CZESŁAW MALINOWSKI\*

# **PROCESSES** IN **THE Cu2S--CuO.CuSO<sup>4</sup> SYSTEM**

### **ANALIZA PROCESÓW W UKŁADZIE Cu2S--CuO.CuSO<sup>4</sup>**

The paper presents research on the course of the reaction in the system of  $Cu<sub>2</sub>S-CuO.CuSO<sub>4</sub>$ . It has been found out that reactions are running through the creation of copper sulphure (I)  $Cu<sub>2</sub>SO<sub>4</sub>$ . The final composition of products depends on the molar ratio of substrates. The processes run with the presence of liquid phase at a specific stage.

W pracy przedstawiono badania przebiegu reakcji w układzie Cu<sub>2</sub>S-CuO.CuSO<sub>4</sub>. Stwierdzono, że reakcje przebiegają poprzez tworzenie się siarczanu miedzi (I)  $Cu<sub>2</sub>SO<sub>4</sub>$ . Końcowy skład produktów reakcji zależy od stosunku molowego substratów. Reakcje zachodzą z wytworzeniem na pewnym etapie fazy ciekłej.

# **1. Introduction**

In the research on the mechanism of metal sulphide deoxidisation, an important role is attributed to the processes between metal sulphides and sulphates. In many cases, the result is indirect products, most often in the form of base sulphates. Occurrence of such products was found out in the systems of  $ZnS-ZnSO_4$ , [1, 2], PbS-PbSO<sub>4</sub> [3, 4] or in mixed systems like  $ZnS-PbSO_4$  [2, 5–8], PbS-ZnSO<sub>4</sub> [4], etc. Base sulphates may react with substrates, making it difficult to selectively differentiate between the successive process stages. This is the case where the temperature range for the original reaction overlaps the temperature range for secondary reactions.

An attempt of interpretation of processes in the system of  $Cu<sub>2</sub>S-CuSO<sub>4</sub>$ , given in [9], indicates that the reaction between copper sulphide (I) and copper sulphate (II)

<sup>\*</sup> WYDZIAŁ METALI NIEŻELAZNYCH, AKADEMIA GÓRNICZO-HUTNICZA, 30-059 KRAKÓW, AL. MICKIEWICZA 30

is occurring with indirect products. One of these may be base copper sulphate (II), resulting from the decomposition of  $CuSO<sub>4</sub>$  sulphate, as well as a result of sulphide deoxidisation with oxygen from sulphate decomposition. Base copper sulphate may in turn react with copper sulphide resulting in copper oxide I) or copper sulphate (I). The thermodynamic analysis of the possible course of reaction in this system, given in figure 1, indicates that reactions between  $Cu<sub>2</sub>S$  and  $CuO.CuSO<sub>4</sub>$  may run even at lower temperatures than reactions between  $Cu<sub>2</sub>S$ and  $CuSO<sub>4</sub>$ . As a result, processes may overlap, and their identification is made more difficult.



Fig. L Change in the reaction free enthalpy in the function of temperature

Literature does not provide much information on the processes in the system of  $Cu<sub>2</sub>S-CuO.CuSO<sub>4</sub>$ . In [10], the results of research over the reactions

 $2Cu_2S+3CuO.CuSO_4 = 5Cu_2O + 5SO_4$ 

are given for the molar ratio corresponding with stoichiometry of the above reaction, in the temperatures of 723, 803 and 873 K. It has been found out that during the reaction, a liquid phase originals in each of the tested temperatures. The final product of the process is  $Cu<sub>2</sub>O$ . Finding of copper sulphate (I)  $Cu<sub>2</sub>SO<sub>4</sub>$  during the reaction seems controversial, whose presence in this system is excluded by R o s e n q vis t [11]. It has to be noticed here that thermodynamic calculations indicate the possibility of this product origination in the indirect stage. Moreover, it has been noticed that the process speed is comparable with the speed of reactions in the system of  $Cu<sub>2</sub>S-CuSO<sub>4</sub>$ .

The purpose of this paper is to attempt an analysis of processes in the system of  $Cu<sub>2</sub>S-CuO.CuSO<sub>4</sub>$  for different molar ratios of their reagents. The phase analysis of products after a specific reaction stage in reference to the thermogravimetric analysis should allow for suggesting the description of the order of the chemical processes.

# **2. Experimental results and their description**

Preparations for research in the processes in the system of  $Cu<sub>2</sub>S-CuO.CuSO<sub>4</sub>$ have been made of the mixture of copper sulphide (I) and base copper sulphate (II) obtained from decomposition of sulphate in the temperature of 900 **K.** The X-ray phase analysis of the decomposition product suggested existence of the  $CuO$ . $CuSO<sub>4</sub>$ phase alone. The material was mixed with  $Cu<sub>2</sub>S$  obtained according to the procedure referred to in paper  $[1]$ , in molar ratios of 1:1, 2:1 and 4:1. The mixtures were first subjected to chemical analysis, the results of which allowed for accurate determination of the molar ratio of sulphide to base sulphate. It was:

- $Cu<sub>2</sub>S+1.007 CuO.CuSO<sub>4</sub>$
- $Cu_2S + 2.041$  CuO.CuSO<sub>4</sub>
- $Cu_2S+3.932$  CuO.CuSO<sub>4</sub>

Then, the preparations were subjected to thermogravimetric analysis in the atmosphere of argon, at linearly increasing temperature with the rate of 10 degree per minute. The temperatures obtained are reported in figures  $2-4$ . The analysis of the course of lines TG and DTA indicates that reactions begin in the temperature of ca. 700 **K,** irrespective of the molar ratio of sulphide to base sulphate. For the preparation of  $Cu_2S + CuO.CuSO_4$ , in the TG line, two ranges of mass loss are noticed, whereas for other molar ratios three ranges are found out. Moreover, for the



Fig. 2. The thermogramme for the preparation of  $Cu_2S + CuO.CuSO_4$ 

preparations of  $Cu_2S + CuO.CuSO_4$  and  $Cu_2S + 2 CuO.CuSO_4$ , in the first stage of the process, two endothermic effects are noticed in the DTA line, with three effects for the  $Cu_2S + 4 CuO.CuSO<sub>4</sub>$  preparation. The shape of DTA peaks is to be taken into account, which appear in the temperature range of ca. 780 K and 850 K. These peaks are very sharp, yet featuring low thermal effects (especially in the preparations



Fig. 3. The thermogramme for the preparation of  $Cu_2S + 2 CuO.CuSO<sub>4</sub>$ 



Fig. 4. The thermogramme for the preparation of  $Cu_2S+4$  CuO.CuSO<sub>4</sub>

of  $Cu_2S + CuO.CuSO_4$  and  $Cu_2S + 2 CuO.CuSO_4$ ). Such peaks are characteristic of physical transformations rather than chemical reactions. Moreover, they appear in the beginning an in the end of the I stage of mass loss, thus not corresponding with mass loss. The analysis of the **DT A** line indicates that the combined endothermic effect increases with the increasing molar ratio of base sulphate to sulphide. This may be different in the partial thermal reactions, corresponding to the I stage of the process.

In order to determine the type of products originating during the processes, samples of the preparations, after a specific reaction stage, were subjected to the X-ray phase analysis. Its results are given in table 1. The phase analysis suggests the possibility of origination of copper sulphate (I)  $Cu<sub>2</sub>SO<sub>4</sub>$  in the process.  $Cu<sub>2</sub>O$  is the final product of the process. For preparations with the molar ratio of sulphate to sulphide of  $2:1$  and  $4:1$ , the CuO phase is also appearing.

TABLE I



Comparison of preparation mass changes: calculated against obtained from TG

When the results of product phase analysis were taken into account after a specific stage of the reaction and the results were included for thermodynamic calculations (figure 1), the following scheme of the reaction course was assumed:

1 stage: 
$$
Cu_2S + 2 CuO.CuSO_4 = Cu_2SO_4 + 2 Cu_2O + 2 SO_2
$$
 (1)

or: 
$$
3 Cu_2 SO_4 + Cu_2 S = 4 Cu_2 O + 4 SO_2
$$
 (2)

and with larger surplus of  $Cu<sub>2</sub>O$ :

2 stage: 
$$
Cu_2S + 2 Cu_2O = 6 Cu + SO_2.
$$
 (3)

With stoichiometry as for the (1) reaction:

$$
2 \text{ stage:} \quad \text{Cu}_2\text{SO}_4 = 2 \text{ CuO} + \text{SO}_2 \tag{4}
$$

3 stage: 2 CuO = Cu<sub>2</sub>O + 
$$
\frac{1}{2}
$$
 O<sub>2</sub> (5)

With surplus  $CuO.CuSO<sub>4</sub>$  in the second stage, apart from the reaction (4) there is a reaction:

$$
CuO.CuSO4 + Cu2O = 4 CuO + SO2
$$
\n(6)

and reaction (5) in the third stage.

The assumed reaction course for preparations with varied molar ratios of reagents was used for calculation of mass changes in the successive process stages. The summary of calculated values with the ones received according to the TG mass change line are given in table 2. When performing the calculations, it was assumed that every stage of the process is running to the very end. For each of the analysed preparations, good conformity was found between experimental values and those from theoretical calculations, especially for the total mass loss. Slight differences of the relative mass change in specific stages may result from the difficulty in the accurate delineation of particular process stages.

TABLE 2



Results of phase analysis of samples after a specific reaction stage

The results of the base analysis and calculations performed based on the assumed course of the processes indicate that reactions in the system of  $Cu<sub>2</sub>S-CuO.CuSO<sub>4</sub>$ run with the indirect product of copper sulphate (I)  $Cu<sub>2</sub>SO<sub>4</sub>$ . The final composition of the reaction products depends on the initial molar ratio of base sulphate to sulphide. For the molar ratio equal to or higher than 2,  $Cu<sub>2</sub>O$  is the final product. With the value lower than 2, mixture of Cu and  $Cu<sub>2</sub>O$  is the final product. One could believe that with high surplus of sulphide, Cu with unprocessed  $Cu<sub>2</sub>S$  will be the final product.

224

## **3. Conclusions**

The process reaction research in the system of  $Cu<sub>2</sub>S-CuO.CuSO<sub>4</sub>$  indicate <sup>a</sup> multi-stage course of the processes, dependent on the molar ratio of reagents. On the basis of phase analysis of samples after a certain stage of reaction, it has been found out that in the I stage of the process, copper sulphate (I)  $Cu<sub>2</sub>SO<sub>4</sub>$  originates, and the final composition of products depends on the molar ratio of substrates. The analyses executed allowed for suggesting the following process course:

- For the molar ration of  $CuO.CuSO<sub>4</sub>: Cu<sub>2</sub>S$  equal 2:
	- I stage  $Cu_2S + 2 CuO.CuSO_4 = Cu_2SO_4 + 2 Cu_2O + 2 SO_2$
- II stage  $Cu_2SO_4 = 2 CuO + SO_2$ <br>III stage  $2 CuO = Cu_2O + \frac{1}{2}O_2$
- 2 CuO = Cu<sub>2</sub>O +  $\frac{1}{2}$ O<sub>2</sub>
- For the molar ration of  $CuO.CuSO<sub>4</sub>:Cu<sub>2</sub>S$  lower than 2: I stage  $Cu_2S + 2 CuO.CuSO_4 = Cu_2SO_4 + 2 Cu_2O + 2 SO_2$ 3  $Cu_2SO_4 + Cu_2S = 4 Cu_2O + 4 SO_2$
- $Cu_2S + 2 Cu_2O = 6 Cu + SO_2$ II stage
- For the molar ration of  $CuO.CuSO<sub>4</sub>:Cu<sub>2</sub>S$  larger than 2:
	- $Cu_2S+2 CuO.CuSO_4 = Cu_2SO_4 + 2 Cu_2O + 2 SO_2$ <sup>I</sup> stage
- $Cu_2SO_4 = 2$  CuO + SO<sub>2</sub> II stage
	- CuO.CuSO<sub>4</sub> + Cu<sub>2</sub>O = 4 CuO + SO<sub>2</sub>
- III stage 2 CuO = Cu<sub>2</sub>O +  $\frac{1}{2}$ O<sub>2</sub>

On the basis of sample appearance, after a specific process stage, it has been found out that processes run at a specific stage with the presence of liquid phase.

The paper financed under KBN State Committee Scientific for Research contract No. 10.10.180.290.

## REFERENCES

- [1] Cz. M a l i n o w s k i, Arch. Hutnictwa 3, Series 29, 353 (1984).
- [2] Cz. Ma <sup>I</sup> <sup>i</sup> <sup>n</sup> <sup>o</sup> wski, ZN AGH, Metalurgia <sup>i</sup> Odlewnictwo **141,** 1456, <sup>I</sup> (1991).
- [3] Cz. Malinowski, Therm. Acta 119, 329 (1987).
- [4] Cz.Ma <sup>I</sup> <sup>i</sup> <sup>n</sup> <sup>o</sup> wski, K. Ma <sup>I</sup> <sup>i</sup> <sup>n</sup> <sup>o</sup> wska, ZN AGH Metalurgia <sup>i</sup> Odlewnictwo, No. 1138, 109, <sup>113</sup> (1987).
- [5] Cz. M a linowski, Archives of Metallurgy 2, 32, 203 (1987).
- [6] Cz. <sup>M</sup> <sup>a</sup> <sup>I</sup> <sup>i</sup> <sup>n</sup> <sup>o</sup> ws <sup>k</sup> i, S. <sup>M</sup> <sup>a</sup> Ie ck i, K. <sup>M</sup> <sup>a</sup> <sup>I</sup> <sup>i</sup> <sup>n</sup> <sup>o</sup> wska, J. Thermal Anal., Series 32, <sup>1747</sup> ( 1987).
- [7] Cz. Ma <sup>I</sup> <sup>i</sup> <sup>n</sup> <sup>o</sup> wski, K. Ma <sup>I</sup> <sup>i</sup> <sup>n</sup> <sup>o</sup> wska, J. <sup>W</sup> <sup>o</sup> It er, XIX Oktobarsko Savctovanije Rudara <sup>i</sup> Metalurga, October 1987, Saopstenija, Knjiga li, <sup>5</sup> <sup>I</sup> 7-524, Bor-Jugoslavia. i Metalurga, October 1987, Saopstenija, Knjiga II, 517—524, Bor-Jugoslavia.<br>[8] Cz. Malinowski, M. Malinowska, S. Małecki, Therm. Acta 275, 117 (1996).
- 
- [9] S. Małecki, Cz. Malinowski, Archives of Metallurgy 44, 4 (1999).
- [IO] W. D. Ponomariev, E.W. Margulis, lzv. AN Kaz. SSR, 3, (1958).
- [11] T. R o s e n q v i s t, Metallurg. Trans., Series 9b, 337 (1978).

REVIEWED BY: PROF. DR HAB. INŻ. MARIAN KUCHARSKI

*Received: 15 March 2000.*